Besoins en mesures et modélisation des états de mer extrêmes pour le dimensionnement des éoliennes en mer

Jean-François Filipot (FEM) Jean.francois.filipot@ite-fem.org

Loads due breaking waves



Slamming loads :

- due to breaking waves
- Severe and impulsive
- Difficult to measure and model

→Slamming loads are similar to what you experience when:
1) you enter water at a beach exposed to breaking waves,

2) or during a "belly flop" at the swimming pool

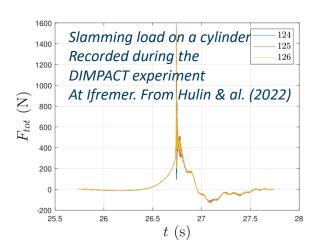




Figure: Top panels : A massive wave slamming La Jument lighthouse. Credit : Air, Vide et Eau. Bottom panel : 2 kids experiencing a slamming load



Effects on Offshore Wind Turbines :

- Local structural damage
- Mode excitation of the tower up to the nacelle
- Run-up : water climbing up along the
- foundation (bottom-fixed or spar type floating OWT)
- Green water : submersion of the substructure

Specifity of Floating Offshore Wind Turbines :

- Floater motion (surge)
- Floater-turbine tilt
- \rightarrow May affect slamming loads
- \rightarrow Need fully aero-hydro-elastic-servo models

(See Derisk project for slamming loads on bottom-fixed OWT)

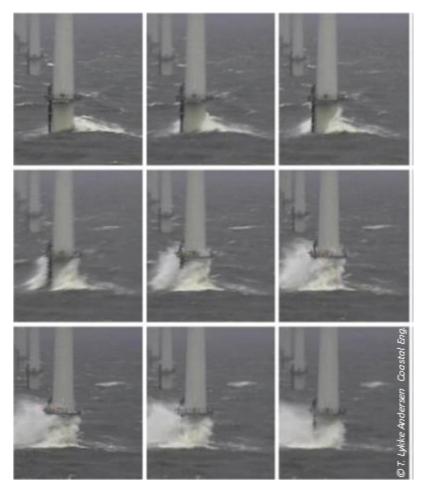
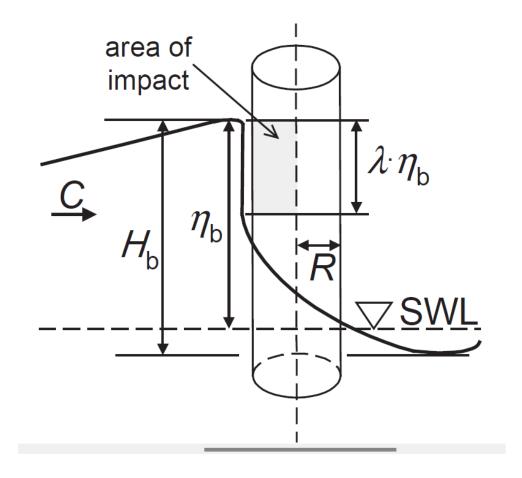


Figure: A breaking wave impacting an OWT on the Horns Reef 1 wind farm, Denmark. From Lykke Andersen et al. [2011].



Need robust statistics on :

- Crest elevation
- Fluid velocity in the crest
- Breaking severity (breaking type)
- Occurrence rate
- In all water depths...
- In the field...





Limitations of buoy measurements

- no valid (enough) breaking criterion from wave buoys
- information in space is needed : shape cannot be derived from time series for highly nonlinear waves
- buoys go around large crests?

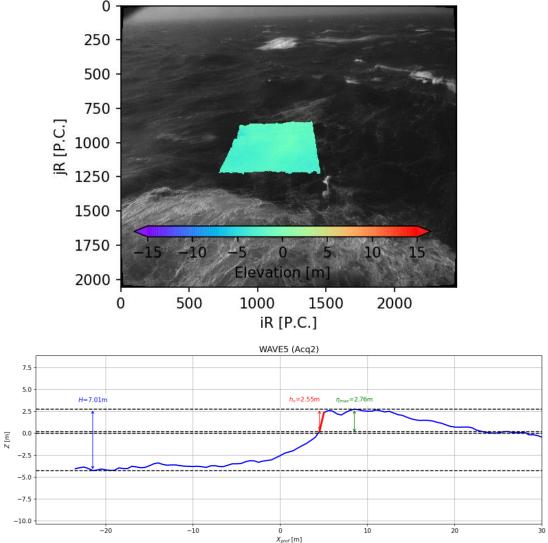


Kinematics and Statistics of Breaking Waves Observed Using SWIFT Buoys

Adam Brown ⁹, Jim Thomson, Ashley Ellenson, Fadia Ticona Rollano, H. Tuba Özkan-Haller, and Merrick C. Haller



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Stereo-Video system :

- Solution No-ambiguous breaking occurrence detection
- Direct estimation of crest shape
- Direct estimation of crest speed
- May survive extreme waves
- Does not work at night, with rain, sunglit
- Heavy data processing
- → Good for research dealing with slamming loads (provides the right input)
 → Bad for generation of robust statistics

Wave profile, from F. Leckler (FEM)

The saturation zone problem

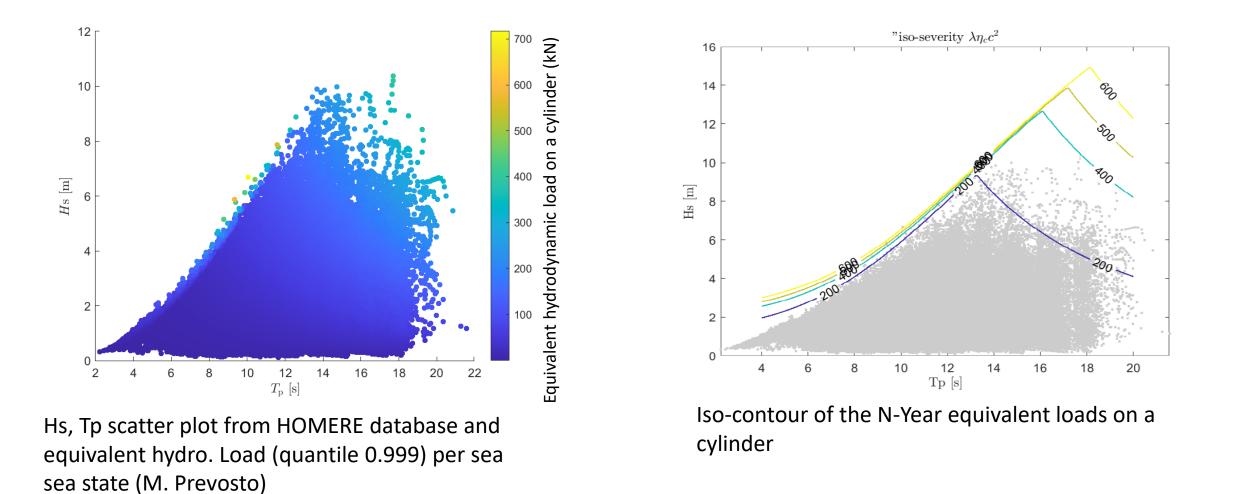


Application to site 50-year F_{0.999} Design sea states Total force model $F_{0.999}/(Hs.c_{01}^2) =$ candidates $\max(0.07, 10.2k_{01}$ Hs - $(3.-2.5e^{-k_{01}d}))$ 50-year iso-severi T = 1, Hs/1.3, Tp T = 3.3, Hs/1.1, Tp T = 7, Hs, Tp T = 20, Hs.1.1, Tp T = 100, Hs.1.1, TpHs [m] $\max(0.07, 10.2\bar{k}Hs - (3. - 2.5e^{-k})$ 10 50 RP yearly max (yrs) $10 T_{01}$ [s] 10 12 14 16 18 20 Tp [s] 4 8 0.4 0.45 0.25 0.5 **FOWT** modeling **Design Load** wave-FOWT information Load model 800 --- SF + Fs Slamming load 1.08 *Γ* = 3.15 - Exp 0.90 (1-λ)η_ν 600 0.72 Clin 400 0.54 F [N] Nonbreaking wave load **U**_{lin} -0.2 E N -0.4 0.36 [5/ 200 $\eta_{\scriptscriptstyle b,\,{\scriptscriptstyle lin}}$ 0.18 ⊃ Γ_{lin} 0.00 -0.6 -0.18 θ -0.36 -200-0.3 -0.2 -0.10.0 t [s] 0.1 0.2 0.3 Ub -0.54 -0.50 -0.25 0.00 0.25 0.50 0.75 1.00 1.25 1.50 X [m]

The DIMPACT method for the design of offshore wind turbines

The saturation zone problem







- How good are spectral wave models for this wave regime?
- In deep/intermediate and shallow water?
- How accurate are the wave buoys measurements in these conditions?
- Can we rely on other source on information (altimeters, SAR) To provide Hs and Tp?

